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EFFECTIVE THERMAL CONDUCTIVITY OF A GLASS FIBERBLANKET STANDARD REFERENCE MATERIAL

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CONTENTS

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of a Glass Fiberblanket Standard Reference Material

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This paper* describes the results of thermal conductivity measurements at temperatures from 84 K to 360 K on a glass fiber-blanket insulation which is intended to be a Standard Reference Material (SRM). The measurements were performed in an atmosphere of dry nitrogen at a pressure near 84 kPa (630 mm Hg). The results are analyzed and compared to literature data for similar material. An annotated bibliography of literature sources is included.

Key words: Glass fiberblanket; insulation; low temperature; standard reference material; thermal conductivity.

Introduction

As part of the National Bureau of Standards - Department of Energy Program

to establish insulation Standard Reference Materials (SRM's), work is continu-

ing on various candidate materials. The results on SRM 1450 (glass fiberboard)

were reported earlier [1]. Results of measurements are reported here for a

specimen of a glass fiberblanket insulation for specimen temperatures covering

the range from 84 K to 360 K, in an atmosphere of dry nitrogen gas at 84 kPa

(630 mm Hg), local atmospheric pressure.

Apparatus and Specimen Characterization

A commercial guarded-hot-plate thermal conductivity instrument was exten-

sively modified [2] to permit efficient use of cryogenic or refrigerated cool-

ants, to obtain greater stability of controlled temperatures, and to achieve

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lower imprecision and uncertainty of measurements. This apparatus was designed to measure heat transfer through a pair of specimens surrounding the horizontal hot plate in the typical double-sided guarded hot plate configuration (ASTM STM C-177).

The pair of specimens studied were disks of nominal 10 cm (4 in) diameter and 2.6 cm (1.0 in) thickness. They were cut from larger slabs measuring approximately 58 cm square as received from the National Bureau of Standards, Office of Standard Reference Materials stock. The pair was chosen on the basis of near equality of area densities (0.0381 g/cm^2 and 0.0383 g/cm^2). The thickness, Δx, of each specimen was determined during the conductivity measurement by three stainless steel spacer tubes positioned at three equidistant points around the perimeter of the guard material. The guard material was similar to that of the specimens with an inside diameter of 10 cm (4 in) and an outside diameter of 20 cm (8 in). The measured thickness was 2.59 cm and the resulting volume density was 14.75 kg/m^3. This thickness was corrected for thermal expansion of the spacers (less than 0.3 percent).

All hot plate/cold plate surfaces facing the specimens were black anodized aluminum. The cold surfaces were electrically heated, temperature-controlled plates, cooled by resistive thermal contacts with fluid-cooled copper plates; thus the cold surfaces of the specimens could be brought to a temperature near that of the coolant, or raised in temperature, as desired. The main heater (metered section) was a disk 10.16 cm in diameter separated by a 1.6 mm gap from the annular guard of 5.1 cm width. A concentric, cylindrical outer guard surrounded the stack of auxiliary heaters, specimens, and main heater. It established a temperature gradient approximating that of the stack about 2 cm away from the stack edge surfaces.

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Temperature controllers were used to regulate conditions in the inner and outer guards and to establish steady temperatures in the auxiliary heaters at the cold sides of the specimens. The offset signal for the inner-guard controller was developed by a 20-pair thermopile of type E thermocouples, with alternate junctions on opposite sides of the gap separating the main and inner-guard heater plates.

Type K thermocouples (32 gauge) for determining temperatures of the specimen faces, positioned at the center and near the gap surrounding the main heater, were varnished to the surfaces of the hot and auxiliary plates over a length of 15 cm. These thermocouples were also thermally tempered by means of 15 cm of wire wrapped and varnished to copper lugs attached to the periphery of the hot and auxiliary plates.

Type K thermocouple wire was calibrated using a calibrated platinum resistance thermometer and baths of liquid helium, liquid nitrogen, dry-ice-and-alcohol, ice-water, room-temperature water, and boiling water. The departures from the standard tabular values* of emf vs. temperature were represented by a 3-term polynomial and a corrected calibration curve was formulated for the particular spools of thermocouple wire used.

The dc power, Q, for the main heater was obtained from a constant current power supply of better than 0.01 percent stability and accuracy. The power in the metered heater was found from the product of voltage drop, V, across the heater and the current, I, through the heater.

Results

Measurements of heat flow and of temperatures of the hot and cold surfaces were performed at mean temperatures from 95 K to 350 K with temperature

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*Thermocouple Reference Tables based on IPTS-68, NBS Monograph 125, March, 1974.

differences of about 25 K (gradient approximately 1 deg/mm). The metered area A_m, was taken to be that contained within the 10.32 cm diameter circle including the main heater and one-half of the surrounding gap. The area through which the metered heat energy flows through the two matched specimens is $2A_m$. This area was corrected for thermal expansion (less than 0.7 percent).

The mean thermal conductivity, $\overline{k}$, was computed according to $\overline{k} = \frac{Q}{A} \frac{\Delta X}{\Delta T} = \frac{VI}{2A_m} \frac{\Delta X}{(T_2-T_1)}$, where T_2 and T_1 are the average hot and cold side temperatures, respectively. The resulting data set of values $\overline{k}$, Q, T_1, and T_2 were then functionally represented using a thermal conductivity integral (TCI) fitting technique* to yield the thermal conductivity as a continuous function of temperature over the range from the lowest value of T_1 (84 K) to the highest value of T_2 (360 K). This resulted in the values of the parameters, A_i in the equation $k = \sum_{i=1}^{4} A_i T^i$. This technique is valid only to the extent that the mechanisms of heat transfer are conductive in nature (as opposed to direct radiation or convection). Deviations from this condition can be detected by searching for systematic trends in the deviations of the fitted data as a function of boundary conditions. This search will be conducted on more extensive data to be published later.

The values of k vs. temperature obtained by means of this technique for the specimens are given in Table 1 and plotted in Fig. 1 (solid line). The values of $\overline{k}$ are also plotted in Fig. 1 (circles) at the mean temperature, $\overline{T}$.

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*Hust, J. G. and Lankford, A., Comments on the Measurement of Thermal Conductivity and Presentation of the Thermal Conductivity Integral Method, to be published.

The fact that the mean values of thermal conductivity, $\bar{k}$, are consistent with the solid line for k at $\bar{T}$ is indicative of the absence of appreciable non-conductive heat transfer mechanisms, i.e., direct radiation and convection. Deviations between $\bar{k}$ and k at $\bar{T}$ can also be caused by non-linear behavior of k vs. T for just conductive heat transfer, but, in this case k vs. T is nearly linear. Table 2 gives the coefficients, A_i, and the range over which the fitted curve is valid. The TCI deviations, $(TCI_{obs} - TCI_{calc}) \times 100/TCI_{obs}$, between the data (obs) and the fitted (calc) curve are given in Fig. 2 as a function of mean temperature. The horizontal bars indicate the temperature range for each measurement and the range of the TCI. A three term polynomial fit showed large systematic deviations from the data but the four term polynomial exhibited mainly random deviations. The remaining small systematic deviations (approximately $\pm$ 1/2 percent) were essentially unchanged from a four term to a seven term polynomial. Further analysis is planned on other data sets to ascertain if these systematic deviations reflect real behavior or experimental error. At about 320 K two triplets of points are shown in Fig. 2 which differ appreciably from the mean ($\pm$ 3 percent). These data are the result of running the apparatus in the single-sided mode, i.e., each triplet is a measure of only one or the other of the two specimens. Further analysis is required to determine if these deviations are caused by specimen variations or by differences in the apparatus configuration.

Other investigators [3-14] have reported similar trends in the dependence of k on temperature for glass fiber insulations over a wide range of densities including our value. The characteristic differences of these insulations,

such as binder or lubricant content, fiber size or atmospheric pressure actually present at each laboratory, are not known in great enough detail to permit definitive statements about the agreement or disagreement between results. Comparisons of literature data [5,7,10,12,14] to our equation are illustrated in Fig. 3. The uncertainty of the present results is estimated to be ± 1 percent. Research on this material is being continued to determine the effects of specimen density and fill gas species and pressure on the effective thermal conductivity. Other parameters such as thickness, plate emittance, and heat flow direction will also be examined to further elucidate the nature of the heat transfer mechanisms present.

Table 1

Thermal conductivity of glass fiberblanket versus temperature based on the fitted results of the present investigation.

T (K)	k (mW/m K)	T (K)	k (mW/m K)
84	8.90	160	17.83
85	9.01	170	19.10
86	9.12	180	20.40
87	9.24	190	21.74
88	9.35	200	23.12
89	9.46	210	24.56
90	9.57	220	26.04
91	9.68	230	27.59
92	9.80	240	29.20
93	9.91	250	30.89
94	10.00	260	32.67
95	10.14	270	34.53
96	10.25	280	36.49
97	10.36	290	38.57
98	10.48	300	40.76
99	10.59	310	43.08
100	10.70	320	45.54
110	11.85	330	48.15
120	13.00	340	50.92
130	14.18	350	53.87
140	15.37	360	57.00
150	16.59		

Table 2

Coefficients of the Least-Squares Fit: $k = \sum\limits_{i=1}^{4} A_i T^i$

$A_1 = 0.986120 \times 10^{-1}$

$A_2 = 0.121313 \times 10^{-3}$

$A_3 = -0.562714 \times 10^{-6}$

$A_4 = 0.190726 \times 10^{-8}$
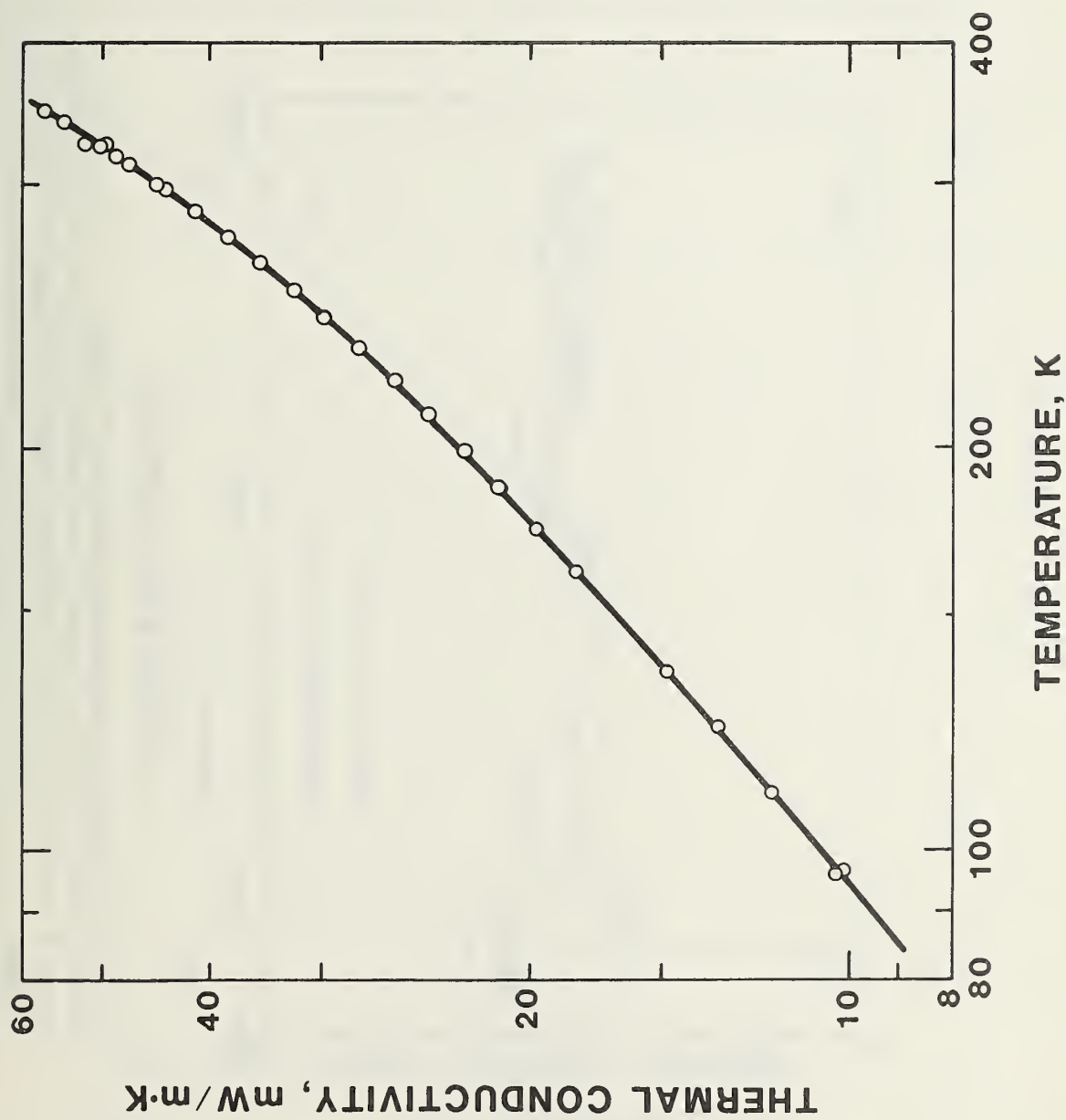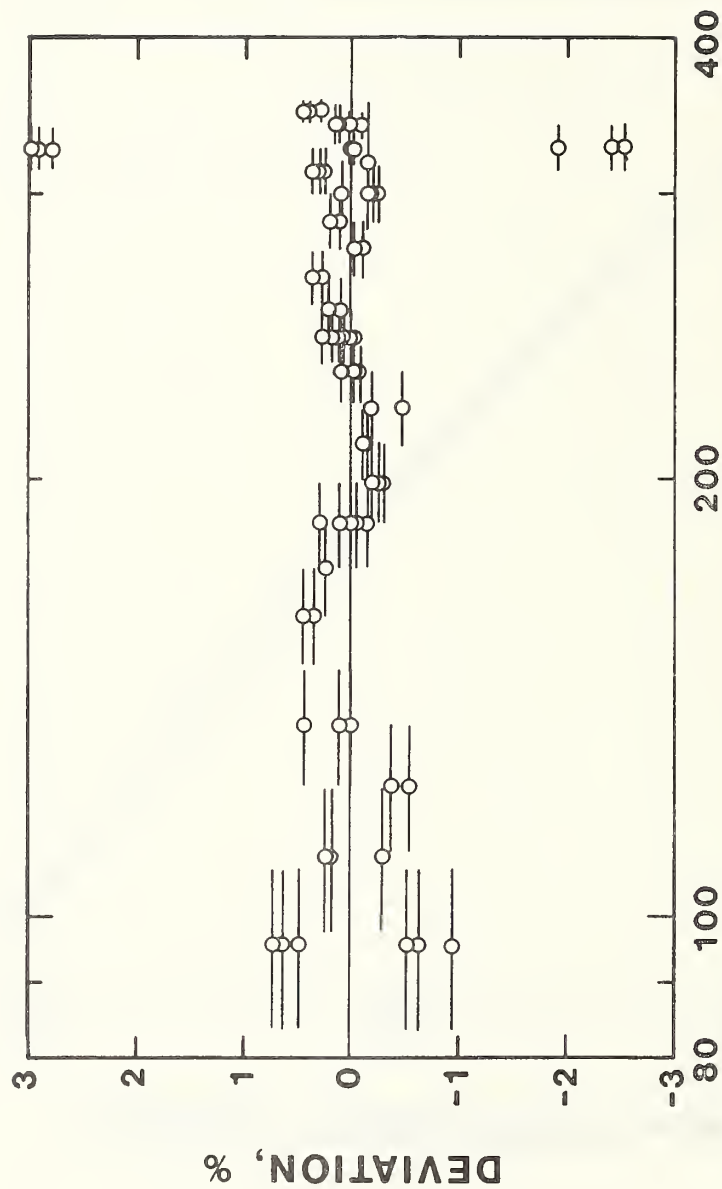
Range: $84K \leq T \leq 360K$

Figure 1 Thermal conductivity data for glass fiberblanket. Solid line shows
results of least squares fit of thermal conductvity integrals, cir-
cles are mean k values plotted at the mean experimental temperatures.

Figure 2 Deviation of observed thermal conductivity integrals (TCI) from cal-
culated values of TCI for glass fiberblanket. Circles show mean tem-
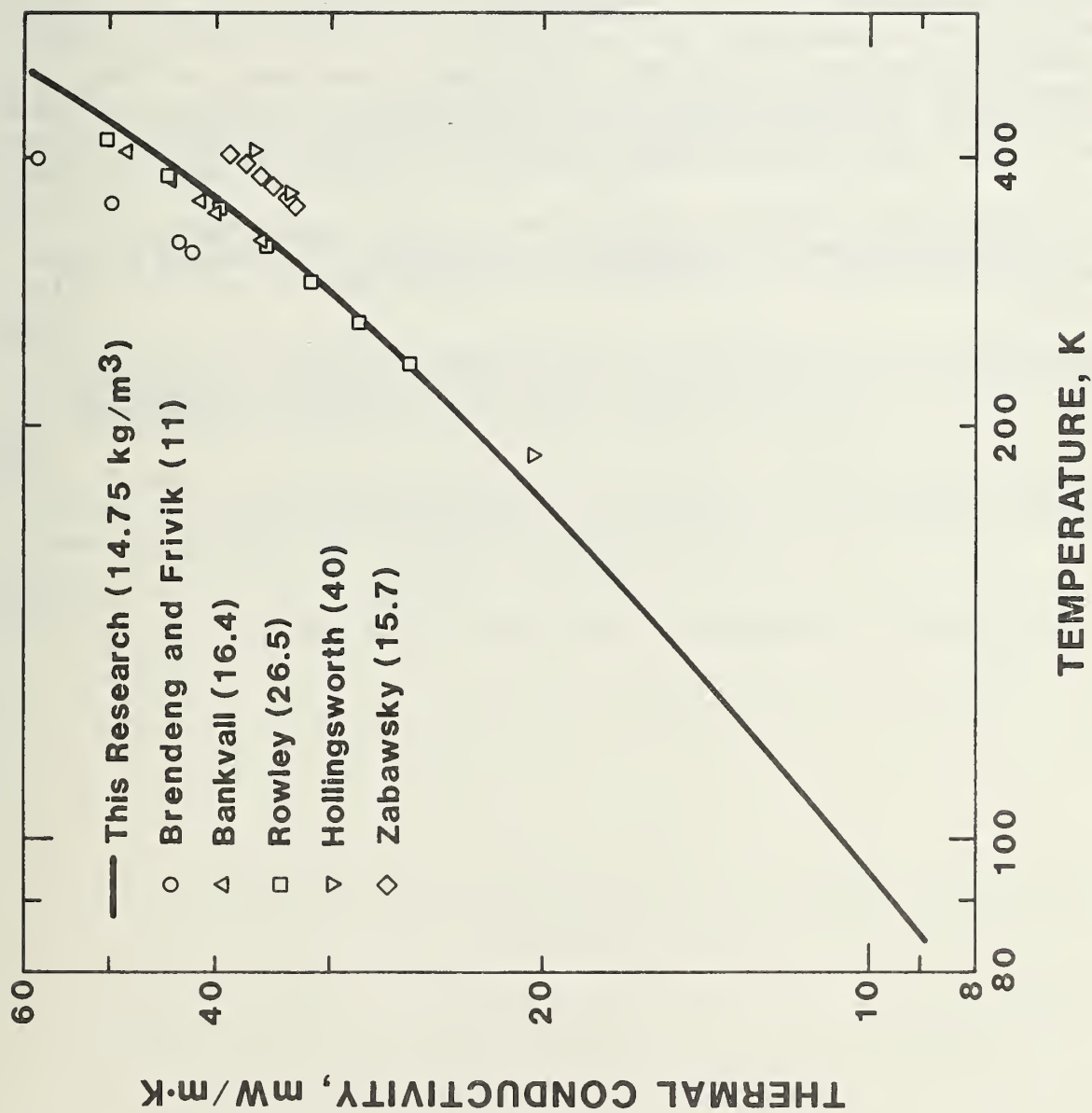perature and horizontal bars indicate temperature span of the mea-
surement.

Figure 3 Comparison of literature data on glass fiberblanket specimens ranging in density from 11 kg/m³ to 40 kg/m³ to our present results.

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References (ANNOTATED BIBLIOGRAPHY)

The references for this document and other papers of interest have been presented in the form of an annotated bibliography as an aid to the reader.

An extensive search has been made of the published literature relating to the effective thermal conductivity of fibrous glass insulation, in the range of densities characteristic of glass fiberblanket. Of special interest to the authors are studies relating to the dependence of k on temperature, density, gas pressure and species of fill gas. The format, given below, for this bibliography is designed to present the conclusions of each paper in a concise manner. Not all papers fit the format in its entirety but the format includes all the relevant types of information found in the majority of papers studied.

It is found that authors' abstracts are not sufficiently detailed in describing specific types of specimen characterization, experimental or theoretical studies and conclusions; therefore abstracts have not been listed in this work.

The units shown in the annotated bibliography are those given in the original article. SI units have been added in parentheses for convenience.

FORMAT FOR ANNOTATED BIBLIOGRAPHY

<u>REFERENCE</u>

AUTHOR, TITLE, CITATION

<u>ANNOTATION</u>

PURPOSE

SPECIMEN
    a) Thickness; b) Density; c) Fill Gas Species/Pressure; d) Fiber Diameter; e) Bonding Agent; f) Other Characterization

APPARATUS
    a) Type; b) Heater Dimensions: Overall/test; c) Plate Orientation or Radial Axis; d) Thermometry; e) Calibration; f) Remarks

THEORY
    a) Physical/Mathematical Models Including Assumptions; b) Calculational Techniques; c) Results

DATA
    a) Temperature Range/Gradient; b) Content of Tables, Figures, and Equations; c) Uncertainty/Imprecision; d) Disputable Corrections to Measurements by Authors; e) Errata (by Author or Reviewer)

ANALYSIS
    a) Comparisons; b) Heat Transfer Mode Separations; c) Conclusions

[1] Smith, D. R. and Hust, J. G., Measurement of Effective Thermal Conductivity of a Glass Fiberboard Standard Reference Material, to be published in Cryogenics; sponsor report No. 773.30-80-2.

PURPOSE
To determine effective thermal conductivities of glass fiberboard materials over a temperature range from cryogenic levels to just above ambient and to develop this material as a standard reference.

APPARATUS
a) guarded hot plate; b) 8 inches (20 cm)/4 inches (10 cm) dia.; c) horizontal; d) type K (Cr-Al) thermocouples; e) calibration measurements agreed to within 1.5%; f) apparatus operated over the range approx. 80 to 350 K.

SPECIMEN
a) 2.59 cm (1 in); b) 123 kg/m^3; c) N$_2$/atmospheric

THEORY
a) k vs T (four term polynomial); b) thermal conductivity integral technique used to fit and calculate k vs T; c) representation of data $\pm$ 0.4% over temperature range.

DATA
a) 87-340 K/1-4 K/mm; b) Table 1 and Figure 1 - k vs T, Figure 2 - deviations from fit of thermal conductivity integrals, Figure 3 - k vs T comparisons with literature data; c) $\pm$ 1% overall

ANALYSIS
a) comparison to literature data

[2] Smith, D. R., Hust, J. G., and Van Poolen, L. J., A Guarded-Hot-Plate Apparatus for Measuring Effective Thermal Conductivity of Insulations Between 80 K and 350 K (to be published as an NBSIR).

PURPOSE
To describe in detail the modifications made to a commercial guarded hot plate apparatus for use as a certification device.

APPARATUS
a) guarded hot plate; b) 8 inches (20 cm)/4 inches (10 cm) dia.; c) horizontal; d) type K (Cr-Al) thermocouples; e) calibration measurements agreed to within 1.5%; f) apparatus operated over the range approx. 80 to 350 K

[3] Allcut, E. A., An Analysis of Heat Transfer Through Thermal Insulating Materials, <u>General Discussion on Heat Transfer</u>, Sep. 1951, IME/ASME pp. 232-235, 486-487 (Inst. Mech. Eng., London, 1951)

PURPOSE
Study influence of radiation and convection on heat transfer in fibrous insulation.

SPECIMEN
b) 1.25 to 3.5 lb/cu ft (20 to 56 kg/m^3); c) air/0.4 to 80 in Hg (1.3 to 270 kPa)

APPARATUS
a) guarded hot plate; b) 8 inches (20 cm); f) enclosed in pressure-vacuum tank

DATA
a) 34 to 96°F/34 to 62°F difference (1 to 36°C/19 to 34°C difference)
b)   Table 1: k vs density for glass wool batts
            2: k vs p for air cell
        3,4,5: k vs p vs T vs density for glass wool batts
            6: % of total heat transmitted by convection
     Figure 1: k vs density for various materials including mineral wool
            2: k vs cell size for Styrofoam
            3: k vs p for various materials
            4: k vs p vs density for glass wool
            5: (p/k) vs p for glass wool
          6,8: convection vs p, and density for glass wool.

ANALYSIS
b) radiation effect is negligible in glass wool blankets exceeding 2 lb/cu ft (32 kg/m^3) density; c) In cellular or granulated materials, k varies almost directly with cell size.

[4]   Allcut, E. A., Properties of Heat Insulating Materials, The Engineering Journal, 514-520 (Nov. 1941)

PURPOSE
A discussion of the character of heat insulating material, the difficulties in determining their relative value experimentally, the effect of air spaces and surface resistance and the possibility of saving fuel by taking advantage of solar radiation and heat stored in the structure of the building itself. An appendix describes a microscopic examination of a number of insulating materials.

SPECIMEN
a) 0.2 to 1.5 in (5 to 38 mm);   b) 1.6 to 5 lb/cu ft (26 to 80 kg/m^3); c) air/atmospheric;   e) 5.5 μm

APPARATUS
a) guarded Hot Plate; b) 8 in (20 cm) square; c)   vertical

DATA
a) 90°F/35 to 200°F/in (32°C/8 to 44°C/cm)
b) Table 1: k vs thickness (density) for three blanket materials (one glass wool).
   Table 2: Heat loss in insulated pipes.
   Figure 1,2: Structure of different fiber boards.
            3: Air leakage in rock wool
            4: Air leakage in fiberboard, different densities.
            6: k vs air pressure for various materials
            8: k vs thickness
            9: k vs density
           11: k vs thickness
           14: fiber-diameter distribution curve.

[5] Bankvall, C., Heat Transfer in Fibrous Materials, J. of Testing and Evaluation, JTEVA, $\underline{1(3)}$, 235-243 (May 1973).

PURPOSE
Mechanisms of heat transfer are calculated theoretically, then verified experimentally by measurements on glass fiber insulation in a specially constructed guarded hot plate apparatus. The author claims the theories give a complete and consistent explanation of the influence of the mechanisms of heat transfer on the effective thermal conductivity of fibrous material.

SPECIMEN
a) 0.5 to 5 cm; b) 15 to 80 kg/m^3; c) air/10^{-3} to 760 mm Hg (0.1 to 100 kPa); d) 5 μm; f) porosity, radiation coefficient.

APPARATUS
a) guarded hot plate, one-sided, rotatable; b) 35 cm diam; c) horizontal

THEORY
a) Fibers in layers at right angles to flow of heat; walls, fibers are "gray", non-transparent bodies; b) Two-phase open-pore model.

$$k_{eff\ gas} = k_{gas} \frac{pL_o}{pL_o + ET}, \quad L_o = \text{inter-fiber distance} = \pi D/4(1-\varepsilon)$$

$$k_{eq.\ fib} = 32(1-\varepsilon)^2 \, sol \Big/ \pi \Big(3 + \frac{\pi}{4(1-\varepsilon)}\Big)$$

$$k_{eff\ rad} = 4\sigma L T_m^3 / (\beta^{-1} + L_o(2/\varepsilon_o - 1)/d) = 4\sigma L_o \beta T_m^3$$

DATA
a) 0 to 56°C; b) Figure 2: Open-pore two-phase model.

        6: Radiation coefficient, β, vs porosity, ε.

        7: k_{fib} vs porosity

        8: β vs ε for different temperatures.

        9: Structural parameter, α, vs porosity, ε.

      10: ε_s vs ε.

      11: Radiational conductivity vs specimen thickness.

      12: k vs T_{mean} for d = 16.4 kg/m^3, low (10^{-3} mm Hg) pressure.

    13, 14: k vs pressure at T_m = 30°C, d = 16.4 and 78.6 kg/m^3

      15: k vs T_m at atmospheric pressure.

      16: Mechanisms of heat transfer in glass fiber.

ANALYSIS
c) All mechanisms involved in transfer by gas must be considered, to be correct in estimating contribution by gas to k_{eff}; d) Conduction in gas contributes largest part of k_{eff} in range 15-80 kg/m^3. Radiation is of greatest importance at low density and leads to large k at low density. Conduction of solids is an important contribution at high density. Increasing temperature leads to larger k, especially at low density where radiation is important.

[6] Bartoli, R. and Laine, P., Thermal Conductivity Measurements of Fiberglass
Panels at Different Temperatures in Various Atmospheres, Supplement to Bull.
of Int'l Institute of Refrig. (Paris) Annexe 1956-2, pp. 233-240 (1956).

PURPOSE
Measurements of thermal conductivity of fiberglass panels in various
gases, at different temperatures.

SPECIMEN
a) 5 cm; b) 33,88,120 kg/m^3; c) air, CO_2, R-12; d) 12 x 10^{-6} m;
e) none

APPARATUS
a) guarded hot plate; c) horizontal; d) copper-constantan thermocouples

DATA
a) -15 to +15°C/26 to 66 K/cm
b) Figures 2,3,4: k vs T, several densities
    air: k_1 = (33.8 + 0.208t)x10-3 kCal/m.h.°C, d_1 = 33 kg/m^3
         k_2 = (26.8 + 0.145t)x10-3 d_2 = 88 kg/m^3
         k_3 = (26.3 + 0.120t)x10-3 d_3 = 120 kg/m^3
    CO_2: k_1 = (23.6 + 0.185t)x10-3
           k_2 = (18.3 + 0.080t)x10-3
    R-12: k_2 = (12.0 + 0.100t)x10-3

ANALYSIS

a) At 0°C $\frac{k_1(CO_2)}{k_1(air)}$ = 0.70, $\frac{k_2(CO_2)}{k_2(air)}$ = 0.69, $\frac{k_2(R-12)}{k_2(air)}$ = 0.45

in good agreement with Verschoor and Greebler, (0.71, 0.71, 0.47, resp.)
at T_m = 66°C.

and k_{1g}(air) = (20.8 + 0.060t)x10^{-3} kCal/m·h·°C ≈ k_{2g} ≈ k_{3g}
    k_{1c}(air) = (13.0 + 0.148t)x10^{-3} kCal/m·h·°C
    k_{2c}(air) = (5.55 + 0.084t)x10^{-3} kCal/m·h·°C
    k_{3c}(air) = (4.75 + 0.058t)x10^{-3} kCal/m·h·°C

[7] Brendeng, E. and Frivik, P. E., New Development in Design of Equipment for Measuring Thermal Conductivity and Heat Flow, Heat Transmission Measurements in Thermal Insulations, ASTM-STP 544, pp. 147-166 (1974).

PURPOSE
This paper describes some of the recent developments in test equipment design and operation.

SPECIMEN
a) 10 cm; b) 11,88 kg/m^3; c) air/atmospheric; f) temperature distribution; influences of convection, emissivity of plates.

APPARATUS
a) guarded hot plate; b) 0.4 m sq.; c) horizontal; d) PRT and thermo-couples; e) measured reference material calibrated at National Physical Laboratory (England)

DATA
a) -5 to 80°C
b) Figure 8: k vs T_m, glass wool and glass fiberboard, 11 and 88 kg/m^3
        9B: k_{eff} vs ΔT, glass wool

[8] Christiansen, R. M. and Hollingsworth, M., Jr., The Performance of Glass
Fiber Insulation Under High Vacuum, <u>Advances in Cryogenic Engineering</u>, <u>4</u>,
141-153 (Plenum, New York, 1960).

PURPOSE
Evaluate technique of partial removal of fill gas from fibrous insulation
to improve thermal performance. Study effective thermal conductivity vs
pressure, density and fiber diameter.

SPECIMEN
a) 0.2-1.8 in. (5 to 45 mm); b) 0.5-15 lb/cu ft. (8 to 240 kg/m^3); c)
air/2 10^{-4} mm Hg to 1 atm (0.03 to 100 kPa); d) 22,45,135, 480 micro-
inches (0.55, 1.1, 3.4, 12 μm); e) heat felting or phenolic resin

APPARATUS
a) heat meter in bell jar; b) 12 in (30 cm) sq; c) vertical; d)
differential thermocouple; e) samples of known conductivity

DATA
a) 75°F/35 to 200°F/in (24°C/8 to 44°C/cm);
b) For a density of 4 lb/ft^3 (64 kg/m^3):
    k(resid. gas + sol.) = 0.0037, k(rad) = 0.0065 at T_m = 75°F (24°C)
    k(resid. gas + sol.) = 0.0018, k(rad) = 0.0016 at T_m = -180°F
    (-118°C)

ANALYSIS
a) Figure 4: k vs pressure (vs fiber diam. vs density)
         6: k vs fiber diam. (vs density, pressure)
         7: Importance of insulation in blocking radiation
         9: component separations
c) For 0.1 mm $\leq$ p $\leq$ 100 mm Hg (0.01 to 13 kPa), finer fiber and higher
density give lower k At low density and high p, optimum fiber diam. is 50
10^{-6} in (130 μm). At low p, higher density not harmful.
Mean free path and average fiber spacing control k.
Optimum density 8 lb/cu ft (130 kg/m^3) at vacuum, 4 lb/cu ft (60
kg/m^3) at atmospheric pressure.
Existence of optimum fiber diameter, predicted by Larkin, confirmed,
because at very low p, k(res) is due to radiation and solid conduction.
When fiber insulation is present at moderately low pressure (0.1 mm, 10
Pa) k is as low as in high vacuum. Fiber insulation necessary to block
radiation between surfaces.

[9] Fournier, D. and Klarsfeld, S., Some recent Experimental Data on Glass Fiber Insulating Materials and Their Use for a Reliable Design of Insulation at Low Temperatures, Heat Transmission Measurements in Thermal Insulations, ASTM STP 544, American Society for Testing and Materials, 223-242 (1974).

PURPOSE

To give theoretical criteria for onset of natural convection in open-pore thermal insulators; measure k; measure permeability to flow of air; guide wall design in minimization of heat transfer.

SPECIMEN

a) 24-28 mm; b) 8-135 kg/m^3; c) air/atmospheric; d) 2.5, 3, 6, 12 μm; f) TEL glass fiber, porosity .93-.997

APPARATUS

a) guarded hot plate; b) 8 in (20 cm)/4 in (10 cm) dia; c) horizontal; d) thermocouple

THEORY

a) right-angle parallelepipedic, tight volume insulating cell, horizontal/vertical orientations; onset of convective motion-filtration Rayleigh Number > 40, for horizontal cells and Rayleigh Number/Aspect Ratio > 4 in vertical cells; c) predict natural convection increases in low temperature ranges

DATA

a) 123-300 K, 20-70 K/in (8 to 28 K/cm);
b) Figure 4: k vs density - fineness ratio as parameter
       5-6: permeability vs density - fineness ratio as parameter
       7-9: k vs T_{mean}, density as parameter
    Other data relating to permeability and convection

ANALYSIS

a) to measurements in a different apparatus - 3% agreement; b) study made of natural convection effect; c) for T < 200 K, density has little influence on k - this is also true of fineness index; TEL glass fiber material for k at temperatures below 198 K behaves similar to cellular plastics and perlite; there are minimum acceptable densities for various thicknesses, temperatures, and fineness ratios to prevent convection

[10] Hollingsworth, M., Jr., An Apparatus for Thermal Conductivity at Cryogenic Temperatures Using a Heat Flow Meter, ASTM STP 411: Thermal Conductivity Measurements of Insulating Materials at Cryogenic Temperatures, 43-51, 1967.

PURPOSE
Evaluate a heat-flow-meter apparatus capable of measuring thermal conductivity of flat insulation specimens at cryogenic temperatures

SPECIMEN
a) 0.5 to 1 inch (1.2 to 2.5 cm);   b) 0.85-3.2 lbm/ft^3 (14 to 51 kg/m^3);   c) air, atmospheric

APPARATUS
a) heat meter in bell jar;   b) 12 x 12 (30 cm) in sq/6 x 6 in (15 cm) sq; c) vertical;   d) copper-constantan thermocouples

DATA
a) -125 to 120°F (-87 to 49°C);   b) Figure 4, k vs T_{mean} for 4 different densities

ANALYSIS
a) results compared with guarded hot plate data from 100-300°F (38 - 149°C); c) apparent good agreement with guarded hot plate data but no accuracy information given because no direct comparisons can be made, i.e., at exactly the same test conditions

[11] Lander, R. M., Gas is an Important Factor in the Thermal Conductivity of Most Insulating Materials, Part II, ASHVE Transactions, 151-168 (1955).

PURPOSE
Describes investigation of the reduction in thermal conductivity of common insulating materials by replacing air with gases of larger molecular weight or fill gas.

SPECIMEN
a) 1 in (25 mm); b) 0.58, 0.78, 1.94, 3.80 lb/ft^3 (9, 12, 31, 61 kg/m^3); c) Air, CO_2, R-12/0.1 μm of Hg to 1 atm (0.01 to 100 kPa)

APPARATUS
a) guarded hot plate; b) 12 in (30 cm) square; c) vertical; d) thermocouples

DATA
a) 100°F mean, 50°F/in (38°C, 11°C/cm)
b) Table 1: k vs fill gas; k(air) vs p; % reduction in heat transfer due to gas substitutions
       2: k vs p for air, CO_2 R-12
       3: k vs % mixture of (CO_2, R-12) with air
       4: k vs T for various gases/densities
       5: Calculated Different Modes of Heat Transfer for three densities, three gases, vs T.
   Figure 7: k vs T for glass wool in air, CO_2, R-12 for varying insulation densities
       9: Gas transferred heat vs T for various fill gases
      11: Heat transferred by radiation/conduction vs density for various T's.

ANALYSIS
b) Fiber conduction/gas transferred heat (conduction)/radiation
c) Major mode of heat transfer is by the fill gas,
   18 to 31% reduction in k if CO_2 replaces air,
   28 to 56% reduction in k if R-12 (CF_2Cl_2) replaces air,
   Conductivity of glass wool is decreased for increasing density (amount of decrease independent of fill gas).
   For practical insulation, radiation is an important mode of heat transfer - conduction through fibers is negligible
   Convection not important except for large volumes of low density insulation.

[12] Rowley, F. B., Jordan, R. C., and Lander, R. M., Thermal Conductivity of Insulating Materials at Low Mean Temperatures, Refrigerating Engineering (J. of ASRE), Vol. 50, No. 6, 541-4, (Dec., 1945).

PURPOSE
An apparatus was built to measure thermal conductivity of common insulating materials at low temperatures

SPECIMEN
a) 0.75 to 1 inch (1.9 to 2.5 cm); b) 1.65-15.7 lbm/ft^3 (26 to 251 kg/m^3); b) air, atmospheric

APPARATUS
a) guarded hot plate; b) 12 x 12 in (30 cm) sq/ 8 x 8 in (20 cm) sq; c) vertical

DATA
a) -60 to 90°F (-51 to 32°C); b) Table 1: for 10 materials of varying density, k vs T_{mean}; Figs. 3-10 k vs T_{mean} at a given density

ANALYSIS
c) Dropping T_{mean}, drops k with the higher density materials having the lower percentage drop

[13] Wilson, F. C., Evacuated and Gas-filled Insulation Systems, Refrig. Eng., pp. 57-60, 102, (Apr. 1957).

PURPOSE
Study effective thermal conductivity in fibrous glass insulation vs species of fill gas, gas pressure, fiber diameter.

SPECIMEN
b) 1,2,9.7,10.9 lb/cu ft (16,32,155,174 kg/m; c) R-12, CO_2, Ne at atmospheric, air at 10 μm Hg to 1 atm (10^{-3} to 100 kPa); d) 27,150,350,500,600, micro-inches (0.68,4,9,12,15 μm); e) none; f) two gas mixtures: H_2-CO_2 and R-12-air.

APPARATUS
a) guarded hot plate; b) specimen in thin bags enclosing fill gas, or apparatus in steel vacuum tank

DATA
a) 75-150°C;
b) Tables I-III: k vs fill gas species at three mean temperatures, four fiber diameters and four densities:

        Figure 1: k vs mol.wt. of fill gas
               2: k vs pressure
             3,4: k vs volume mixture % of CO_2, H_2 and of R-12, air
               5: k vs density for various fiber diameters

ANALYSIS
c) to reduce thermal conductivity by choice of fill gas, use any mol.wt. $\geq$ 50,
k is greater for coarser fibers,
k is at residual level for $p \leq 0.01$ mm of Hg (1 Pa),
k increases less than linearly from value for high-mol.wt. fill gas when
  diluted (air),
Optimum density for 150 micro-inch (4 μm) fiber is 2.5 lb/cu ft (40 kg/m^3).

[14] Zabawsky, Z., An Improved Guarded Hot Plate Thermal Conductivity Apparatus with Automatic Controls, ASTM Symposium on Thermal Conductivity Measurements, STP No. 217, 3-17 (1957).

PURPOSE
To describe an apparatus constructed according to ASTM Standard C177-45 but with additional changes to allow measurement of k within 1% of values determined by the National Bureau of Standards.

SPECIMEN
a) 0.5 to 1.5 in (13 to 38 mm); b) 9.6, 15.7, and 68.2 kg/m^3

APPARATUS
a) guarded hot plate; c) horizontal; d) thermocouples; f) heater to guard $\pm$ 0.004°F (0.002°C), cold plate control $\pm$ 0.05°F (0.03°C), reproducibility $\pm$ 0.5%.

DATA
a) 60-110°F (16 to 43°C); b) Fig. 14 k vs T for three fiberglass materials

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Standard Reference Material

5. AUTHOR(S)

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6. PERFORMING ORGANIZATION (If joint or other than NBS, see instructions)

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8. Type of Report & Period Covered

10. SUPPLEMENTARY NOTES

☐ Document describes a computer program; SF-185, FIPS Software Summary, is attached.

11. ABSTRACT (A 200-word or less factual summary of most significant information. If document includes a significant bibliography or literature survey, mention it here)

This paper describes the results of thermal conductivity measurements at temperatures from 84 K to 360 K on a glass fiberblanket insulation which is intended to be a Standard Reference Material (SRM). The measurements were performed in an atmosphere of dry nitrogen at a pressure near 84 kPa (630 mm Hg). The results are analyzed and compared to literature data for similar material. An annotated bibliography of literature sources is included.

12. KEY WORDS (Six to twelve entries; alphabetical order; capitalize only proper names; and separate key words by semicolons)

Glass fiberblanket; insulation; low temperature; standard reference material; thermal conductivity.